## RSE-M

### IN-SERVICE INSPECTION RULES FOR MECHANICAL COMPONENTS OF PWR NUCLEAR ISLANDS.

2016 EDITION

1st Erratum – October 2020

#### **Afcen**

French Association for Design, Construction and In-Service Inspection Rules for Nuclear Island Components

AFCEN - Association governed by the French Law of 1<sup>st</sup> July, 1901

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#### **NOTE TO THE USERS**

This document proposes modification which correspond to a translation error in the RSE-M 2016 English edition. The following page is to be replaced:

- Volume II – Appendix 5.4 – Page 31

RSE-M – 2016 Edition Appendix 5.4

If  $L_{r}^{^{\star}} < L_{r} \leq 1,$  a new value for  $K_{r}$  is determined by a linear interpolation between  $K_r(L_r^*)$  and  $K_r(L_r=1)$ :

$$K_r = K_r(L_r^*) + \frac{K_r(L_r = 1) - K_r(L_r^*)}{1 - L_r^*}(L_r - L_r^*)$$

 $K_{r}\left(L_{r}^{*}\right) = \left\{\frac{\mathsf{E}\varepsilon_{\mathsf{ref}}\left(L_{r}^{*}\mathsf{S}_{\mathsf{y}}\right)}{L_{r}^{*}\mathsf{S}_{\mathsf{y}}} + 0.5\frac{\left(L_{r}^{*}\right)^{2}}{\left(L_{r}^{*}\right)^{2} + 1}\right\}^{-\frac{1}{2}}$ where

 $K_r(L_r = 1) = \left\{ \frac{E\epsilon_{ref}(S_y)}{S} + 0.25 \right\}^{-\frac{1}{2}}$ and

d) J is calculated by the formula: 
$$\frac{K_J - \left[\frac{\sigma_{nor}}{\sigma_{no}}\right]^2 \left[\psi + \frac{\varepsilon_{ref}}{\sigma_{ref}/E}\right]}{1}$$

### $J_s = J_{el.} \frac{1}{K^2}.$

#### IV.4.1.1.2 $J_S$ CLC OPTION – STRAIGHT PIPE - LONGITUDINAL SURFACE **BREAKING DEFECT**

a) L<sub>r</sub> is calculated using the following expression:

$$L_r = \sqrt{\left[\frac{p}{q_p \mu_{ep}}\right]^2 + \left[\frac{m_1}{q_p \mu_{em1}}\right]^2 + \left[\frac{m_2}{q_m}\right]^2}$$

where p,  $n_1$ ,  $m_1$  and  $m_2$  are normalized loads:

$$p = \frac{\sqrt{3}}{2} \frac{Pr_m}{tS_v} \qquad \qquad m_1 = \frac{\sqrt{3}}{2} \frac{M_1}{\pi r_m^2 tS_v} \qquad \qquad m_2 = \frac{M_2}{4 r_m^2 tS_v}$$

P: internal pressure

M₁: torsional moment M₂: bending moment

- if  $m_2 \neq 0$  and  $p \leq 0.5$ , this expression is valid for  $L_r \leq 1.4$ ;
- if  $m_2 \neq 0$  and p > 0.5, this expression is valid for  $L_r \leq 1.2$ .

If only the applied moment modulus |M| is known, it is assumed that:  $M_1 = |M| \text{ and } M_2 = 0.$ 

The significance and value of coefficients  $q_m$ ,  $q_p$ ,  $\mu_{em1}$  and  $\mu_{ep}$  are given in compendium (VII).

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### IN-SERVICE INSPECTION RULES FOR MECHANICAL COMPONENTS OF PWR NUCLEAR ISLANDS.

2017 EDITION

1st Erratum – October 2020

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- Volume II – Appendix 5.4 – Page 31

### RSE-M

## IN-SERVICE INSPECTION, INSTALLATION AND MAINTENANCE RULES FOR MECHANICAL COMPONENTS OF PWR

2018 EDITION

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- Volume II – Appendix 5.4 – Page 31

RSE-M – 2018 Edition Appendix 5.4

If  $L_r^* < L_r \le 1$ , a new value for  $K_r$  is determined by a linear interpolation between  $K_r(L_r^*)$  and  $K_r(L_r=1)$ :

$$K_r = K_r(L_r^*) + \frac{K_r(L_r = 1) - K_r(L_r^*)}{1 - L_r^*}(L_r - L_r^*)$$

 $K_{r}\left(L_{r}^{\star}\right) = \left\{\frac{\mathsf{E}\varepsilon_{\mathsf{ref}}\left(L_{r}^{\star}\mathsf{S}_{\mathsf{y}}\right)}{L_{r}^{\star}\mathsf{S}_{\mathsf{y}}} + 0.5\frac{\left(L_{r}^{\star}\right)^{2}}{\left(L_{r}^{\star}\right)^{2} + 1}\right\}^{-\frac{1}{2}}$ where

 $K_r(L_r = 1) = \left\{ \frac{E\epsilon_{ref}(S_y)}{S} + 0.25 \right\}^{-\frac{1}{2}}$ and

$$\underline{K_{J}} = \left[\frac{\sigma_{nor}}{\sigma_{no}}\right]^{2} \left[\psi + \frac{\varepsilon_{ref}}{\sigma_{ref}/E}\right]$$

# d) J is calculated by the formula: $\frac{K_J - \left[\frac{\sigma_{nor}}{\sigma_{no}}\right]^2 \left[\psi + \frac{\varepsilon_{ref}}{\sigma_{ref}/E}\right]}{\left[\psi + \frac{\varepsilon_{ref}}{\sigma_{ref}/E}\right]}$ $J_s = J_{el.} \frac{1}{K^2} \, .$

#### IV.4.1.1.2 $J_S$ CLC OPTION – STRAIGHT PIPE - LONGITUDINAL SURFACE **BREAKING DEFECT**

a) L<sub>r</sub> is calculated using the following expression:

$$L_r = \sqrt{\left[\frac{p}{q_p \mu_{ep}}\right]^2 + \left[\frac{m_1}{q_p \mu_{em1}}\right]^2 + \left[\frac{m_2}{q_m}\right]^2}$$

where p,  $n_1$ ,  $m_1$  and  $m_2$  are normalized loads:

$$p = \frac{\sqrt{3}}{2} \frac{Pr_m}{tS_y} \qquad \qquad m_1 = \frac{\sqrt{3}}{2} \frac{M_1}{\pi r_m^2 tS_y} \qquad \qquad m_2 = \frac{M_2}{4 r_m^2 tS_y}$$

P: internal pressure

M₁: torsional moment M₂: bending moment

- if  $m_2 \neq 0$  and  $p \leq 0.5$ , this expression is valid for  $L_r \leq 1.4$ ;
- if  $m_2 \neq 0$  and p > 0.5, this expression is valid for  $L_r \leq 1.2$ .

If only the applied moment modulus |M| is known, it is assumed that:  $M_1 = |M| \text{ and } M_2 = 0.$ 

The significance and value of coefficients  $q_m$ ,  $q_p$ ,  $\mu_{em1}$  and  $\mu_{ep}$  are given in compendium (VII).

RSE-M – 2017 Edition Appendix 5.4

If  $L_r^* < L_r \le 1$ , a new value for  $K_r$  is determined by a linear interpolation between  $K_r(L_r^*)$  and  $K_r(L_r=1)$ :

$$K_r = K_r(L_r^*) + \frac{K_r(L_r = 1) - K_r(L_r^*)}{1 - L_r^*}(L_r - L_r^*)$$

 $K_{r}\left(L_{r}^{\star}\right) = \left\{\frac{\mathsf{E}\varepsilon_{\mathsf{ref}}\left(L_{r}^{\star}\mathsf{S}_{\mathsf{y}}\right)}{L_{r}^{\star}\mathsf{S}_{\mathsf{y}}} + 0.5\frac{\left(L_{r}^{\star}\right)^{2}}{\left(L_{r}^{\star}\right)^{2} + 1}\right\}^{-\frac{1}{2}}$ where

 $K_r(L_r = 1) = \left\{ \frac{E\epsilon_{ref}(S_y)}{S} + 0.25 \right\}^{-\frac{1}{2}}$ and

$$\underline{K_J} = \left[\frac{\sigma_{nor}}{\sigma_{no}}\right]^2 \cdot \left[\psi + \frac{\varepsilon_{ref}}{\sigma_{ref}/E}\right]$$

# d) J is calculated by the formula: $\frac{K_J - \left[\frac{\sigma_{nor}}{\sigma_{no}}\right]^2 \left[\psi + \frac{\varepsilon_{ref}}{\sigma_{ref}/E}\right]}{\left[\psi + \frac{\varepsilon_{ref}}{\sigma_{ref}/E}\right]}$ $J_s = J_{el.} \frac{1}{K^2} \, .$

#### IV.4.1.1.2 $J_S$ CLC OPTION – STRAIGHT PIPE - LONGITUDINAL SURFACE **BREAKING DEFECT**

a) L<sub>r</sub> is calculated using the following expression:

$$L_r = \sqrt{\left[\frac{p}{q_p \mu_{ep}}\right]^2 + \left[\frac{m_1}{q_p \mu_{em1}}\right]^2 + \left[\frac{m_2}{q_m}\right]^2}$$

where p,  $n_1$ ,  $m_1$  and  $m_2$  are normalized loads:

$$p = \frac{\sqrt{3}}{2} \frac{Pr_m}{tS_y} \qquad \qquad m_1 = \frac{\sqrt{3}}{2} \frac{M_1}{\pi r_m^2 tS_y} \qquad \qquad m_2 = \frac{M_2}{4 r_m^2 tS_y}$$

P: internal pressure

M₁: torsional moment M₂: bending moment

- if  $m_2 \neq 0$  and  $p \leq 0.5$ , this expression is valid for  $L_r \leq 1.4$ ;
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If only the applied moment modulus |M| is known, it is assumed that:  $M_1 = |M| \text{ and } M_2 = 0.$ 

The significance and value of coefficients  $q_m$ ,  $q_p$ ,  $\mu_{em1}$  and  $\mu_{ep}$  are given in compendium (VII).

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